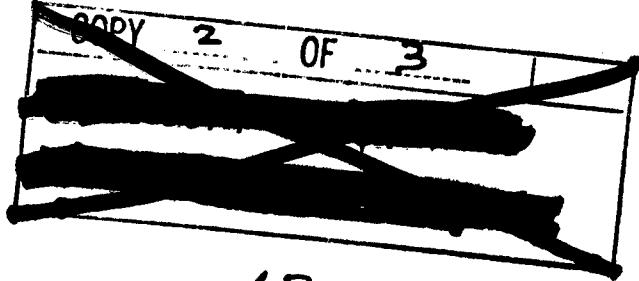


AD 605502



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R 326

Technical Report

AIR-FILTER SHIELDING  
FOR EMERGENCY SHELTERS

19 August 1964

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U. S. NAVAL CIVIL ENGINEERING LABORATORY

Port Hueneme, California

20041122042

# AIR-FILTER SHIELDING FOR EMERGENCY SHELTERS

Y-F011-05-02-344

Type C

by

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## ABSTRACT

Experiments were conducted to show which particle sizes of fallout falling from altitudes of 10,000 feet or more would be drawn into a typically protected shelter air intake. Results indicated that practically no particles over 60 microns in diameter would be captured. Some particles in the 30- to 60-micron-diameter size range were captured, and almost all particles below 30 microns in diameter were captured. Calculations made on two fallout-size distributions and three radioactivity levels indicate no significant hazard from material collected on the shelter air filters. Side-opening blast-closure devices, such as the AMF and OCD units, require additional protection to keep fallout from being captured by the high velocities at the inlet.

Shelters close to atomic blasts are likely to be subject to dangerous amounts of all sizes of particles coming from lower altitudes. These shelters must have all intakes closed during the danger period.

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results obtained by those who have applied the information.

## INTRODUCTION

Certain emergency shelters have extensive air-filtration systems designed to remove CBR contaminants from the shelter's incoming air. When the filters are located near the main shelter area, a potential radiation hazard may exist if the filters become heavily loaded with radioactive fallout particles. The objective of this task is to investigate the extent of this hazard and, if a sufficient hazard exists, to design a filter shield.

## SHELTER FILTER SYSTEMS

Blast-protected shelters with CBR collective protection have ventilation filters capable of removing nearly 100 percent of all particulate material. The filter system contains an impingement prefilter capable of removing 5- to about 100-micron particles with high efficiency, and an absolute filter capable of removing nearly all particles of all sizes. The prefilter serves to minimize the dust load on the absolute filter. Although the prefilter is less effective on particles over about 50 microns, because inertia tends to carry them through, these larger particles are usually excluded by the intake and by sedimentation in the duct work.

## FALLOUT CHARACTERISTICS

To accurately assess the hazard from accumulation of radioactive particles in the air and filter system, it is necessary to know the characteristics of the fallout that the system will be subjected to. Fallout occurs with surface and shallow sub-surface bursts whenever soil is mixed with the fireball. High-altitude bursts and deep-underground bursts do not cause any significant amount of local fallout. In most cases of surface or shallow sub-surface bursts, the contaminated soil will rise to an elevation of 10,000 to 100,000 feet, and the pattern of fallout can be predicted on the basis of average winds and falling times of variously sized particles. Definite percentages of the different particle sizes are usually used to simulate fallout from these high altitudes. A weight of material producing a fallout of about 10, 33, and 100 grams per square foot has usually been used by the Naval Radiological Defense Laboratory in fallout studies to simulate fallout corresponding to 300, 1000, and 3000 r per hour one-hour reference dose rates (detector three feet above infinite plane).

The size groups shown later are associated with these fallout levels, although variation in size groups will occur with different weapon-burst geometries and climatic conditions. Close-in fallout from partially underground bursts may not be separated into discrete size groups. In this case, large quantities of particles under 50 microns in diameter may be drawn into protected intakes. Consequently, the conclusions of this report, which depend on the falling-time separation of fallout into particle-size groups, are not valid for close-in shelters subjected to large quantities of fallout and ordinary dust of mixed sizes. Because of this and other dangers, such as fire and heat, close-in shelters normally keep all intakes closed or blowers shut off until the early blast effects have passed.

## SUCTION-CAPTURE EXPERIMENTS

To obtain data on the actual amount of fallout that will be drawn into an air intake from a high altitude, several experiments were run. The test setup shown in Figure 1 was constructed for these experiments. The intake was designed as a model to represent a typical protected inlet that does not permit a direct downward or sidewise path into the air duct.

The air system was operated at 600 cfm through the 8-inch duct for an average velocity of about 1800 fpm. A removable filter was located in the duct system to retain all particles sucked into the intake. The filter was weighed before and after experiments to obtain data on how much simulant was sucked in.

The overhead rack shown in Figure 1 was about 7 feet above the inlet, and calculation showed this height to be adequate for typical particle sizes to reach approximate terminal velocities by the time they fell to the level of the intake. Approximate terminal velocities for several sizes are shown in Table I.

The first fallout simulant was a quantity of sand with the size distribution shown in Table II. This distribution is based on Naval Radiological Defense Laboratory (NRDL) test data from "Operation Redwing,"<sup>1</sup> and was used for this test because it contains some particles below 50 microns in diameter. The mixture was discharged from the spreader on the overhead rack. Although the terminal velocities would indicate that at least some of these smaller particles would be captured in the intake, the contrary proved true and none were drawn in. It is considered possible that the smaller particles were adhering to the larger ones and being carried past the inlet with them.

A mixture of 1- to 50-micron particles was then dropped from a 200-mesh strainer past the inlet, and it could be visually observed that practically 100 percent of this material falling near the inlet was captured. Since it appeared that the

50-micron size was the approximate dividing line between capture and dropping past the inlet, a new batch of material with sizes ranging from 30 to 60 microns was used for an additional test. With this material dropping past the inlet, it could be seen that particles falling within 6 inches of the edge of the conical cap were drawn into the inlet. Beyond this point, there was little or no capture.

During this test, 204 grams of material was dropped over an area of about 9 square feet. The capture area was found to cover about 5 square feet, so that  $5/9(204)$ , equal to 113 grams, fell through the capture area. When the filter was weighed, it showed that 42 grams had actually passed into the duct. Although refined testing might indicate more precisely what percentage of various sizes would be captured under ideal conditions, the results of these tests are considered to show that all particles over 60 microns will fall past a conical-capped inlet, approximately 40 percent in the 30- to 60-micron range will be sucked in, and nearly 100 percent of particles smaller than 30 microns passing through an inlet-velocity zone of about 200 fpm will be captured.

### Significance of Inlet Particle Capture

The size distribution of fallout particles at a given location will be variable, but the amount of radioactivity involved is roughly proportional to the cumulative weight of each particle-size group. Table III shows a calculation of the amount of radioactivity that will be sucked in under several conditions, assuming that the percentage of particles captured at the inlet will be similar to the results of the suction-capture experiment. Fallout radioactivity levels of 300, 3000, and 10,000 r per hour are used as a basis for total weights of materials involved in the calculations in Table IV. Two particle-size distributions are used. One is that developed by NRDL and used by the U. S. Army Nuclear Defense Laboratory at Camp McCoy.<sup>2</sup> It is shown in Table IV. The other is the Redwing distribution from Table II. The Redwing distribution has a greater percentage of material in the smaller sizes. Since no particles over 60 microns in diameter were captured in the experimental tests, all particles larger than that are grouped as 60+ microns. A 10-hour period for the fallout to arrive is used in the analysis of the 300 r/hr reference dose rate.

Table IV shows that very little of the 150-300 micron NRDL simulant would be drawn in. Consequently, little or no radioactivity would accumulate on the filter, and no hazard would exist for the condition of a 600-cfm protected inlet. The Redwing distribution has a larger weight of material in the small-size ranges that will be captured, but Table III shows that the amount of radioactivity that will collect on the filter is small in all cases. The rate at 4 feet from collected fallout on the filter is smaller than that being received through the shelter walls. Nevertheless, some hazard would exist to anyone having to change the prefilter when it

was newly contaminated. However, this filter would not necessarily require immediate changing, since for the 600-cfm unit only about 65 grams of fallout would collect on the filter, and this type of filter in a 20- by 20-inch size can hold several hundred grams. Unless the filter was very dirty before the fallout arrival, it could be left in place until the activity had decayed for a few days. However, it could safely be changed about one day after contamination if gloves were worn.

## DISCUSSION

The experimental data showing that protected intakes will not capture any significant portion of fallout particles larger than about 60 microns is a reconfirmation of accepted design practice in shelter intakes. When the data is applied to particles from 150 - 300 microns, usually assumed as typical for fallout reference levels of 1000 to 3000 r per hour, there is practically no radioactivity collected on the filter and no danger to shelter inhabitants.

When fallout particles of the size that would come from a more distant detonation point reach an air intake, a larger percentage of them would be drawn in. Assuming that the smaller particles would not arrive until 10 hours after the detonation, the hazard to occupants is quite low.

Some increase of collected radioactivity will occur for larger sizes of ventilation systems. The hazard would increase from about 0.0125 r per hour indicated for a 600-cfm M9A1 system to about 0.025 r per hour at a 4-foot distance. This hazard is still relatively low and would decay to a fraction of this in 24 hours.

The importance of having a protected air intake should not be overlooked and is emphasized in NAVDOCKS P-81.<sup>3</sup> The AMF and Mosler blast closures have side openings with moderately high air-entrance velocities. The 36-inch AMF closures have an entrance velocity of about 1250 fpm at 10,000 cfm. When used as air intakes, these closures should be protected. Such protection exists in the entrance tunnel or can be provided by a blast-resistant shield above the valve, extending about a foot beyond the valve circumference.

## CONCLUSIONS AND RECOMMENDATIONS

1. Fallout consisting of particles larger than about 60 microns will not be captured by protected air intakes.

2. A considerable percentage of fallout that occurs in the 30 - 60 micron range will be captured by a protected air intake, but the amount of radioactivity involved does not indicate a hazard to shelter occupants.
3. It is concluded that special shielding is not required for intake air filters.
4. All shelter air intakes should be protected against direct downward or sidewise entrance of fallout.
5. Precaution. The findings of this report should not be applied to close-in shelters receiving large amounts of fallout immediately after a blast.

#### REFERENCES

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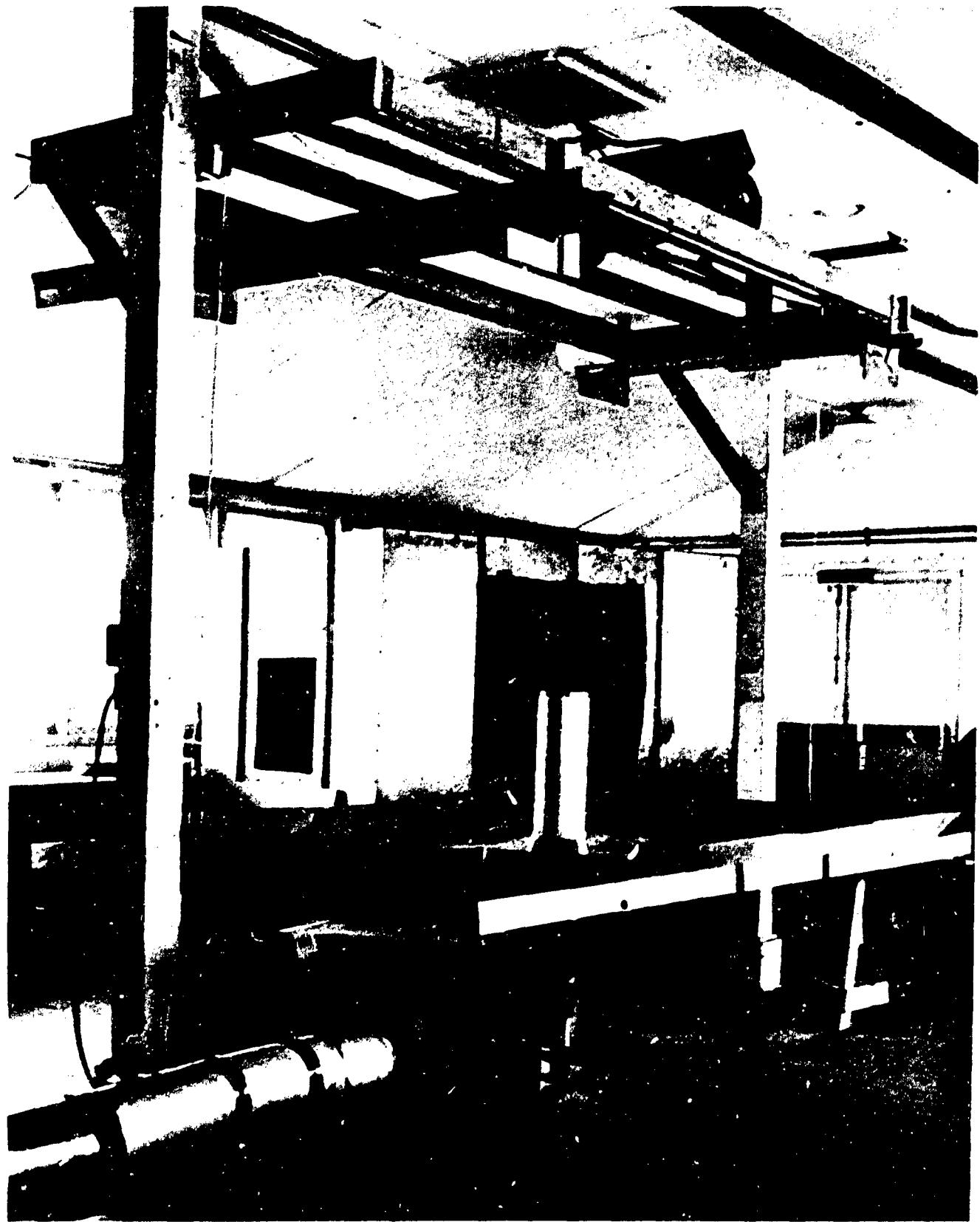


Figure 1. Test setup with sheet metal model intake for suction-capture experiments.

Table I. Terminal Falling Velocities for Various Fallout-Particle Sizes

Particle Diameter (microns)	Terminal Velocity <sup>4</sup> (fpm)
50	16
75	80
100	120
125	165
150	210
200	275
400	660

Table II. Particle Distribution Derived From Operation Redwing Data

Particle Diameter (microns)	Percent of Total by Weight
30 - 60	11
61 - 102	17
103 - 145	18
146 - 200	28
201 - 315	25
316 - 382	1

**Table III. Filter Hazard Calculation**

Particle Size (microns)	Percent by Weight	Curies to 5 ft <sup>2</sup>	Particles Captured (%)	Curies Captured on Filter	Rate <sup>1</sup> /4 ft From Filter (r/hr)	Dose Rate From Outside, Protective Factor 1000 (r/hr)
300 r/hr (1 hr); 10 gm/ft <sup>2</sup> ; 0.162 curies/ft <sup>2</sup> at 10 hr						
60+	89	0.71 (10 hr)	0	0	0	0
30 - 60	11	0.09 (10 hr)	37	0.033	0.0125	0.018
30-	0	0	100	0	0	0
3000 r/hr (1 hr); 100 gm/ft <sup>2</sup> ; 27 curies/ft <sup>2</sup> at 1 hr						
60+	99.8	134.73 (1 hr)	0	0	0	0
30 - 60	0.2	0.27 (1 hr)	37	0.10	0.04	3
30-	0	0	100	0	0	0
10,000 r/hr (1 hr); 330 gm/ft <sup>2</sup> ; 90 curies/ft <sup>2</sup> at 1 hr						
60+	99.8	449.1 (1 hr)	0	0	0	0
30 - 60	0.2	0.90 (1 hr)	37	0.33	0.125	10
30-	0	0	100	0	0	0

1/ Dose rate calculated from  $D = 6CE/R^2$ , where  $R$  = distance from source in feet;  $E$  = million electron volts;  $C$  = radioactivity in curies.

2/ Based on 0.009 curies/ft<sup>2</sup>/r/hr at 1 hour.

Table IV. NRDL-NDL-McCOY Simulant Size Distribution

Particle Diameter (microns)	Percent of Total by Weight
44 - 88	0.18
88 - 105	0.10
105 - 149	1.21
149 - 297	56.10
297 - 350	30.38
350+	12.00

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